

# Relative Permeability Correlations

## Subtopics:

[Two-Phase Correlations](#)

[Corey](#)

[Honarpour](#)

[Generalized Corey](#)

[Three-Phase Correlations](#)

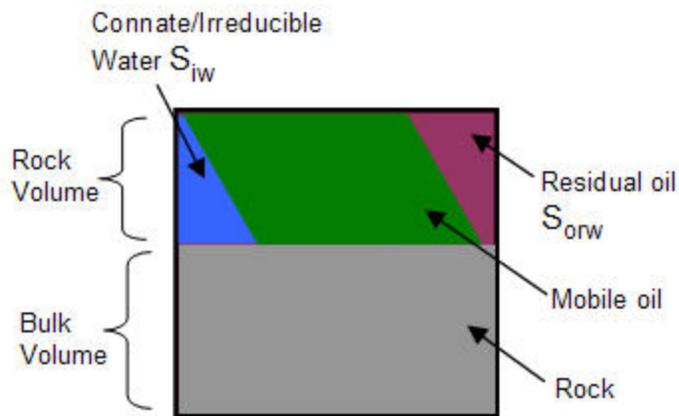
[Stone I](#)

[Stone II](#)

[Baker](#)

## Two-Phase Correlations

In a two-phase system, the fluids consist of oil and water, oil and gas, or gas and water. An example of an oil-water system is shown below:



## Corey

This model assumes the wetting and non-wetting phase-relative permeabilities to be independent of the saturations of the other phases and requires only a single suite of gas/oil-relative permeability data.

### Water / Oil System

$$k_{ro} = \left[ \frac{1 - S_o}{1 - S_{iw}} \right]^2 \left[ 1 - \left( \frac{S_o - S_{iw}}{1 - S_{iw}} \right)^2 \right]$$

$$k_{rw} = \left[ \frac{S_w - S_{iw}}{1 - S_{iw}} \right]^4$$

### Gas / Oil System

$$k_{rg} = \left[ \frac{S_g}{1 - S_{org}} \right]^2 \left[ 1 - \left( \frac{1 - S_g - S_{org}}{1 - S_{org}} \right)^2 \right]$$

$$k_{ro} = \left[ \frac{S_o - S_{org}}{1 - S_{org}} \right]^4$$

### Gas / Water System

$$k_{rg} = \left[ \frac{S_g}{1 - S_{iw}} \right]^2 \left[ 1 - \left( \frac{1 - S_g - S_{iw}}{1 - S_{iw}} \right)^2 \right]$$

$$k_{rw} = \left[ \frac{S_w - S_{iw}}{1 - S_{iw}} \right]^4$$

## Honarpour

Developed using data from oil and gas fields in the continental US, Alaska, Canada, Libya, Iran, Argentina and the United Arab Republic.

### Sandstone

#### Water Wet

$$k_{rw} = 0.035388 \left[ \frac{S_w - S_{iw}}{1 - S_{iw} - S_{orw}} \right] - 0.0108074 \left[ \frac{S_w - S_{orw}}{1 - S_{iw} - S_{orw}} \right]^{2.9} + 0.56556 (S_w)^{3.6} (S_w - S_{iw})$$

### Intermediate Wet

$$k_{rw} = 1.5814 \left[ \frac{S_w - S_{iw}}{1 - S_{iw}} \right]^{1.91} - 0.58617 \left[ \frac{S_w - S_{orw}}{1 - S_{iw} - S_{orw}} \right]^{2.9} (S_w - S_{iw}) + 1.2484 \phi (1 - S_{iw})(S_w - S_{iw})$$

### Any Wettability

$$k_{row} = 0.76067 \left[ \frac{\left( \frac{S_o}{1 - S_{iw}} \right) - S_{or}}{1 - S_{orw}} \right]^{1.8} \left[ \frac{S_o - S_{orw}}{1 - S_{iw} - S_{orw}} \right]^{2.0} + 2.6318 \phi (1 - S_{orw})(S_o - S_{orw})$$

$$k_{rog} = 0.98372 \left[ \frac{S_o}{1 - S_{iw}} \right]^4 \left[ \frac{S_o - S_{org}}{1 - S_{iw} - S_{org}} \right]^2$$

$$k_{rg} = 1.1072 \left[ \frac{S_g - S_{gc}}{1 - S_{iw}} \right]^2 k_{rgro} + 2.7794 S_{org} \left[ \frac{S_g - S_{gc}}{1 - S_{iw}} \right] k_{rgro}$$

## Limestone

### Water Wet

$$k_{rw} = 0.0020525 \left[ \frac{S_w - S_{iw}}{\phi^{2.15}} \right] - 0.051371 \left[ \frac{S_w - S_{iw}}{k_{abs}^{0.43}} \right]$$

### Intermediate Wet

$$k_{rw} = 0.29986 \left[ \frac{S_w - S_{iw}}{1 - S_{iw}} \right] - 0.32797 \left[ \frac{S_w - S_{orw}}{1 - S_{iw} - S_{orw}} \right]^2 (S_w - S_{iw}) + 0.413259 \left[ \frac{S_w - S_{iw}}{1 - S_{iw} - S_{orw}} \right]^4$$

### Any Wettability

$$k_{row} = 1.2624 \left[ \frac{S_o - S_{orw}}{1 - S_{orw}} \right] \left[ \frac{S_w - S_{iw}}{1 - S_{iw} - S_{orw}} \right]^2$$

$$k_{rog} = 0.93752 \left[ \frac{S_o}{1 - S_{iw}} \right]^4 \left[ \frac{S_o - S_{org}}{1 - S_{iw} - S_{org}} \right]^2$$

$$k_{rg} = 1.8655 S_g \left[ \frac{S_g - S_{gc}}{1 - S_{iw}} \right] k_{rgro} + 8.0053 (S_{org})^2 \left[ \frac{S_g - S_{gc}}{1 - S_{iw}} \right] - 0.025890 (S_g - S_{gc}) \left[ \frac{1 - S_{iw} - S_{org} - S_{gc}}{1 - S_{iw}} \right]^2 \left[ 1 - \frac{1 - S_{iw} - S_{org} - S_{gc}}{1 - S_{iw}} \right]^2 \left[ \frac{k_{abs}}{\phi} \right]^{0.5}$$

## Generalized Corey

Similar to the Corey correlation, but developed for a wider range of rock and wettability characteristics. This correlation can be used to change the endpoints of water-oil and gas-liquid relative permeability curves while still retaining the shape of the curves.

### Gas / Oil System

$$k_{rog} = k_{rocw} \left[ \frac{S_o - S_{iw} - S_{org}}{1 - S_{iw} - S_{org}} \right]^{n_{og}}$$

$$k_{rgo} = k_{rgro} \left[ \frac{S_g - S_{go}}{1 - S_{gc} - S_{iw} - S_{org}} \right]^{n_g}$$

### Gas / Water System

$$k_{rg} = k_{rgcw} \left[ \frac{S_g - S_{gc}}{1 - S_{gc} - S_{iw}} \right]^{n_g}$$

$$k_{rw} = k_{rwc} \left[ \frac{S_w - S_{iw}}{1 - S_{iw}} \right]^{n_w}$$

## Water / Oil System

$$k_{ro} = k_{rocw} \left[ \frac{1 - S_w - S_{orw}}{1 - S_{iw} - S_{orw}} \right]^{n_{ow}}$$

$$k_{rw} = k_{rwrw} \left[ \frac{S_w - S_{iw}}{1 - S_{iw} - S_{orw}} \right]^{n_w}$$

## Three-Phase Correlations

Three-phase relative permeability can be generated from the two-phase relative permeability curves of the oil-water system and the relative permeability curves of the gas-oil system. The two-phase curves represent the end curves when either the gas saturation or water saturation equals zero.

### Stone I

This probability model estimates three-phase permeability data from laboratory measured two-phase data. It uses the channel flow theory in porous media to obtain a simple result for determining the relative permeability to oil in the presence of water and gas flow. The model implies that water-relative permeability and water-oil capillary pressure in three-phase systems are functions of water saturation alone, irrespective of the relative saturations of oil and gas. Similarly, the gas-phase relative permeability and gas-oil capillary pressure are the same functions for gas saturation in the three-phase system as in the two-phase gas-oil system.

Stone I is widely used in the industry as the benchmark for oil simulation. It is a better predictor than Stone 2 in low oil saturation regions, is more appropriate for water-wet systems, and is not suited for intermediate wet systems.

$$S_o^* = \frac{S_o - S_{orw}}{1 - S_{iw} - S_{orw}}$$

$$S_w^* = \frac{S_w - S_{iw}}{1 - S_{iw} - S_{orw}}$$

$$S_g^* = \frac{S_g}{1 - S_{iw} - S_{orw}}$$

$$k_{ro} = k_{rocw} S_o^* \left[ \frac{k_{row}(@ S_w)}{k_{rocw}(1 - S_w^*)} \right] \left[ \frac{k_{rog}(@ S_g)}{k_{rocw}(1 - S_g^*)} \right]$$

## Stone II

Stone's Model II is a modified version of Stone I. It is a better predictor than Stone 1 in high-oil saturation regions. It is more appropriate for water-wet systems and is not suited for intermediate wet systems.

$$k_{ro} = k_{rocw} \left[ \left( \frac{k_{row}}{k_{rocw}} + k_{rw} \right) \left( \frac{k_{rog}}{k_{rocw}} + k_{rg} \right) - (k_{rw} + k_{rg}) \right]$$

## Baker

Baker's three-phase model is based on saturation-weighted interpolation between the two-phase relative permeability values. It is well suited for intermediate wet or oil-wet systems.

$$k_{ro} = \frac{(S_w - S_{iw})(k_{rocw}) + (S_g - S_{gc})(k_{rog})}{(S_w - S_{iw}) + (S_g - S_{gc})}$$